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超双疏表面的制备及应用进展



分享本文

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摘要: 自然界中的超疏水/超疏油现象吸引了表界面科学、微纳制造及纳米涂层等多学科领域研究者的广泛关注, 在人们的生产生活中展现出了巨大的应用前景。本文聚焦于具有微纳粗糙结构的超双疏表面发展现状, 从基本润湿性理论出发, 介绍了超双疏表面微观粗糙结构的主要类型和降低表面能的原理, 探讨了表面微观粗糙结构和化学改性与润湿性之间的关系, 并归纳了制备超双疏表面的主要方法。最后, 总结了超双疏表面的主要应用现状, 分析了超双疏表面目前存在的不足和缺陷, 并对其未来的发展方向进行了展望。

关键词: 超双疏; 超疏水; 润湿性; 表面微/纳结构; 功能涂层

中图分类号: TQ638; TB332 **文献标志码:** A **文章编号:** 1000-3851(2024)11-5876-18

Progress in the preparation and application of superamphiphobic surface

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Abstract: Superhydrophobic/superoleophobic phenomenon in nature have attracted extensive attention from researchers in surface interface science, micro-nano manufacturing, nano coating and other fields, and have shown great application prospects in people's production and life. Based on the basic wettability theory, this paper introduces the main types of micro-nano rough structures on superoleophobic surfaces and the principle of reducing surface energy. The relationship between the micro-nano rough structure, chemical modification, and wettability also be explored, and the main methods for preparing superamphiphobic surfaces are summarized. Finally, the main applications status of the superamphiphobic surface are summarized, and the shortcomings and defects of the superamphiphobic surface are analyzed. Likewise, the future development direction of the superamphiphobic surface is prospected.

Keywords: superamphiphobic; superhydrophobic; wettability; surface micro/nano-structure; functional coating

超疏水/超疏油表面的研究涵盖了物理、化学、表面与界面、流体力学、纳米材料、仿生学等多个学科领域。1997年, Barthlott等^[1]阐述了荷叶表面的自清洁机制, 为超疏水表面的进一步开发及应用提供了思路和启发。2002年, 江雷院士团队^[2]从微观结构、化学成分等方面进一步揭示了荷叶表面实现超疏水性能的深层机制, 为超疏水表面的设计和制备奠定了理论基础。此后, 具有疏液

性能的特殊浸润表面制备及其应用研究逐渐受到业内研究者的广泛关注^[3-5]。单一的超疏水表面在遭受油污等黏附时, 其表面疏水性便会失效, 使表面的使用受到诸多限制^[6-8]。因此研发兼具超疏水和超疏油特性的超双疏表面, 是拓展超疏水表面应用领域及推进疏液表面发展应用的重要趋势^[9-12]。

为了实现材料表面的超双疏特性, 国内外研究者开展了大量研究工作, 并取得了较好的研究

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进展。例如, 2011年, Xiong等^[13]设计了一种由氟化嵌段和凝胶嵌段共同形成的双嵌段共聚物, 共聚物与二氧化硅颗粒结合后形成的涂层表现出了超双疏特性; 2015年, Lee等^[14]在蘑菇状微柱阵列结构的表面沉积纳米颗粒, 实现了透明超双疏表面的制备; 至2016年, Tian等^[15]确立了超双疏表面的设计原则, 为其研发提供了理论指导。此后, 超双疏表面的制备技术得到迅速发展, 其制备工艺也逐渐多样化。例如, 采用纳秒激光纹理加工与氟烷基硅烷基自组装相结合的方法, 制备了具有潜在工业应用价值的超双疏表面^[8]; Wu等^[16]采用单向摩擦加热处理方法制备的聚合物薄膜或涂层, 兼具高透明性和超疏液性, 在自清洁太阳能电池板及防指纹透明保护膜等方面具有较好的潜在应用前景; Li等^[17]结合光刻、反应离子刻蚀等技术制备了具有凹角结构的超双疏表面, 并研究了拉普拉斯压力对超双疏性能的影响, 为耐久性超双疏表面的设计提供了参考。

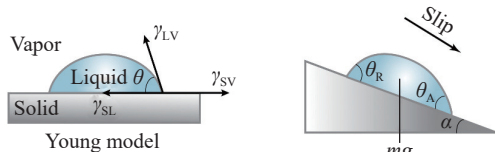
由于超双疏表面具有疏液^[18-19]、防污^[20]、耐腐蚀^[21]、防结冰^[22]、减阻^[23]等特性, 在防腐蚀^[24]、自清洁与抗污^[25-26]、防冰^[27]等方面展现出了广阔的应用前景和巨大的经济效益。近年来该领域的研究涵盖了表面的微纳结构设计^[28]、表面能的降低^[29]、多领域应用的探索^[30]、涂层稳定性和耐久性的提高等方面^[31-33]。其中存在的基础科学问题和应用难题, 至今仍需深入的探索和研究。

本文针对近年来的研究成果进行梳理, 介绍了基本的润湿理论, 总结了3种超双疏表面的微结构类型, 归纳了超双疏表面的制备方法, 分析了超双疏表面在防腐蚀、防污与自清洁和防除冰方面的应用前景。最后, 对超双疏表面目前存在的问题和未来的发展方向进行了总结。

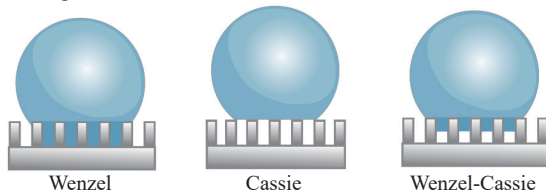
1 润湿理论

接触角(CA)是指当液滴位于水平表面时, 在固、液、气三相交界处, 自固-液界面经过液体内部到气-液界面之间的夹角^[34], 如图1(a)所示。当液滴放置在倾斜的斜面时, 液滴在重力作用下刚好滑动时, 所对应的倾角为滑动角(SA)或滚动角(RA), 如图1(b)所示。CA和SA是表征表面润湿性的两个主要参数, 可作为评价表面疏液性的重要参考。对于超疏水表面, 其表面的水接触角(WCA)大于 150° , 滑动角(SA)小于 10° 。如果该表面同时对水和油类液体都表现出极好的排斥性

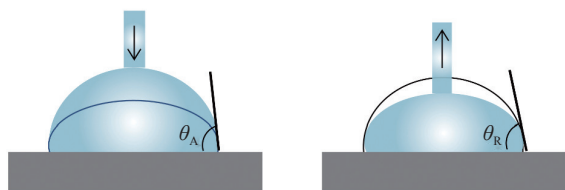
(a) Contact angle and slip angle



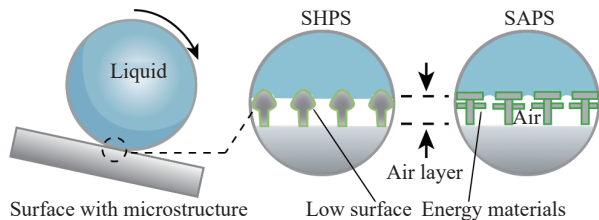
(b) Wetting model



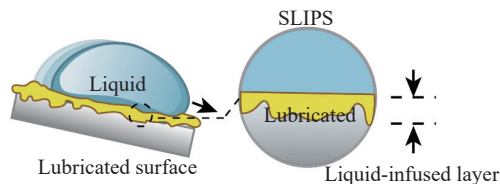
(c) Contact angle hysteresis



(d) Air-mediated surface



(e) Liquid-infused surface



γ_{SV} —Surface tension of solid-gas interfaces; γ_{SL} —Surface tension of solid-liquid interfaces; γ_{LV} —Surface tension of liquid-gas interfaces; m —Mass of the droplet; g —Gravitational constant; θ_R —Receding contact angle; θ_A —Advancing contact angle; α —Inclination of a bevel

图1 润湿性理论: (a) 基于杨氏模型理论的接触角和滑动角; (b) 超疏水表面(SHPS)与超双疏表面(SAPS); (c) 接触角滞后; (d) Wenzel模型、Cassie-Baxter模型、混合模型示意图; (e) 光滑液体注入多孔表面(SLIPS)

Fig. 1 Wettability theory: (a) Contact angle and slip angle base on Young model; (b) Air-mediated superhydrophobic surface (SHPS) or superamphiphobic surface (SAPS); (c) Contact angle hysteresis; (d) Schematic diagram of Wenzel model, Cassie-Baxter model and Mixed model; (e) Slippery lubricant-infused porous surface (SLIPS)

(WCA和油接触角(OCA)均大于 150° 且SA小于 10°), 则称为超双疏表面^[18, 35]。

润湿性理论是解释超疏水/超疏油现象的基础。润湿理论中的杨氏模型、Wenzel模型、Cassie-Baxter模型、Furmidge动态润湿性方程等(其理

论模型如图 1(a)、1(b) 所示), 可由以下方程来描述。

对于被液滴润湿的理想固体表面, CA 的大小取决于其物理化学性质 (即表面张力)^[36]:

$$\gamma_{SV} = \gamma_{SL} + \gamma_{LV} \cos \theta_Y \quad (1)$$

式中: γ 为表面张力 (或表面自由能), 其下标 SV、SL、LV 分别代表固-气、固-液和液-气界面; θ_Y 称为杨氏接触角。

考虑了粗糙度效应影响后得到的 Wenzel 润湿性方程为^[37]

$$r\gamma_{SV} = r\gamma_{SL} + \gamma_{LV} \cos \theta_W \quad (2)$$

式中: θ_W 为表观接触角 (粗糙固体表面的接触角); r 为粗糙度系数。

针对复合材料界面相互作用后的 Cassie-Baxter 润湿性方程为^[38]

$$\cos \theta_{B-C} = f_1 \cos \theta_1 - f_2 \quad (3)$$

在考虑固体表面和空气的接触角时, 更普遍的方程形式为

$$\cos \theta_{B-C} = f_1 \cos \theta_1 + f_2 \cos \theta_2 \quad (4)$$

其中: θ_{B-C} 为 Cassie-Baxter 模型中的表观接触角; f_1 和 f_2 分别为复合接触界面中固-液界面和液-气界面的面积分数; θ_1 和 θ_2 分别代表液体与平坦固体表面和空气的接触角。此外, 当超疏水表面被低表面张力的有机液体污染、腐蚀后, 其空腔容易渗入液体, 导致表面润湿状态从 Cassie-Baxter 状态向 Wenzel 状态转变^[39-40]。表面润湿性状态处在介于 Wenzel 态和 Cassie-Baxter 态的状态时, 则称为混合润湿状态, 也称过渡状态^[41-45], 其混合状态时的接触角 θ_{mix} 可以用以下方程进行描述^[46]:

$$\cos \theta_{mix} = r f_1 \cos \theta_Y + f_1 - 1 \quad (5)$$

前述的润湿性方程描述了静止状态下的润湿性。对于动态表面润湿性, 也可以采用接触角滞后 (CAH) 进行评估。图 1(c) 所示的是利用悬滴法测量 CAH 的过程, CAH 数值上等于前进角 (ACA) 与后退角 (RCA) 的差值。物体表面的动态润湿性可由 Furmidge 方程确定^[47]:

$$mg \sin \alpha = \gamma_{LV} L (\cos \theta_A - \cos \theta_R) \quad (6)$$

式中: m 、 L 分别为液滴的质量和接触长度; g 为引力常数; α 为液滴的滑动角; θ_A 和 θ_R 分别为前进角和后退角。较小的 CAH 意味着液滴所受到的表面黏附力较低, 容易脱离材料表面, 具有优异的疏液性能。因此, Furmidge 动态润湿性方程是

对静态润湿性理论的补充。

表面的润湿状态由固体表面的微观几何形貌和化学成分共同决定^[48-50]。超疏水/超疏油表面的微纳结构间隙中存在一层“气垫”, 可以减小液体与固体表面的接触面积, 进而降低液滴与粗糙表面的接触黏附力。同时, 在该粗糙表面进一步添加低表面能物质, 可提高其表面的疏液性。相比于超疏水表面, 超双疏涂层需要更复杂的微纳结构和更低的表面自由能^[51-52]。如图 1(d) 所示, 超双疏表面通常需要具备复杂的多层次微结构, 增加对液滴向上抬升的拉普拉斯压力, 并结合较低表面能的物质进一步降低其表面能, 从而实现超双疏性能。因此, 合理的表面化学成分和特定的微结构是其制备的关键^[15]。此外, 光滑液体注入多孔表面也是疏液表面的一类, 如图 1(e) 所示, 在具有多孔粗糙结构中注入低表面能润滑油并形成光滑表面, 对互不相溶液体表现出了低黏附性和易滑动性, 表现出超疏水性或双疏特性^[53-54]。

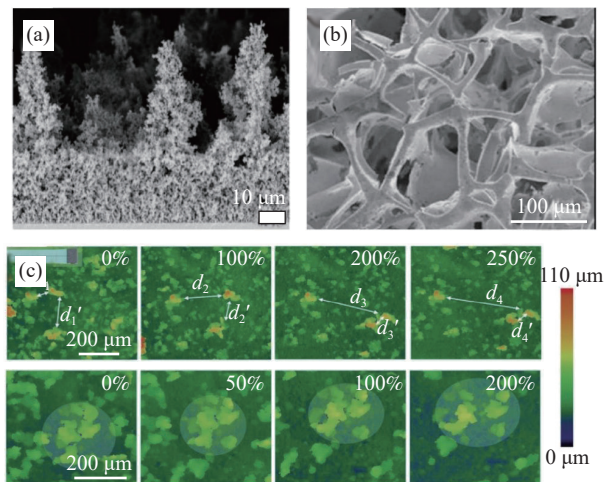
2 表面微观结构

根据润湿性理论, 表面的微/纳米结构能够在液体和固体微纳结构之间形成气垫, 减小固体与液体的接触面积, 使表、界面保持良好的 Cassie 态。“凹角结构”或“层次结构”等微观结构使基体表面能够形成更加稳定的气垫, 承受更大的液体渗透压力^[55-57]。此外, 凹角结构的曲率弧度产生的向上的拉普拉斯压力能够提高表面的疏液性, 表现出更高的接触角, 为超双疏表面的构造奠定良好的基础条件^[17]。

2.1 多孔结构

多孔结构是一种常见且普遍的微观结构, 可以通过化学腐蚀、浸涂、喷涂等方法在基体表面进行构筑。多孔结构中丰富的空隙中可以存留大量的空气, 以保持良好的 Cassie 状态。图 2(a) 显示了微观尺度的枝晶状多孔结构及密集的纳米颗粒在枝晶状结构上形成的纳米级孔隙^[58], 枝晶结构与直径小于 100 nm 的纳米孔隙的结合, 提供了 Cassie 态所需的微结构基础, 提供了良好的超双疏条件。Li 等^[59] 通过聚多巴胺与 SiO₂ 纳米颗粒结合在基体表面构造了网络状的多孔结构, 其表面形貌如图 2(b) 所示。多孔结构参数对于表面或涂层的疏液性能至关重要, 只有在微尺度多孔网络结构具备一定的孔径和孔高及空隙壁厚时, 才能保证更多的空气滞留于涂层的孔隙中并保持

良好的 Cassie 态, 从而具备从超疏水转变到超双疏的可能性。Zhou 等^[60]以聚二甲基硅氧烷 (PDMS) 层为粘结剂, 通过在可拉伸基底上喷涂预先制备好的硅纳米丝, 以形成纳米多孔粗糙表面, 经氟化改性处理后制成可拉伸的超双疏表面。在拉伸和收缩的过程中, 不同方向的纳米颗粒团簇间距会增加或减少, 但多孔的粗糙结构不会被破坏。如图 2(c) 所示, 即使在高拉伸应变 (约 225%) 和 1 000 次拉伸释放循环下, 表面也能保持稳定的水和正十六烷的超双疏性。由于多孔结构的空隙大小和间距难以精确控制, 难以保持其性能稳定性, 常用于超疏水表面的构建。不过多孔结构可与其他类型的结构进行组合, 以获得耐久的疏液性能。



d, d' —Spacing of two clusters under different strain

图 2 多孔结构表面微观形貌: (a) 液体火焰喷涂表面的 SEM 图像^[58]; (b) 多孔表面的 SEM 图像^[59]; (c) 经过拉伸后压缩微结构的重新排列过程^[60]

Fig. 2 Surface microstructure of porous structure: (a) SEM image of liquid flame spray surfaces^[58]; (b) SEM images of porous surface^[59]; (c) SEM image of rearranging process of the compacted microstructures after stretching^[60]

2.2 凹角结构

凹角结构 (Re-entrant structure) 可以有效地阻止外部液体渗透到结构内部的空腔中, 从而形成稳定的 Cassie 状态, 表现出疏液特性。凹角结构已经发展出包括锐边、棉花糖状、T-形、微柱梯形和悬垂结构等在内的多种类型^[61-63], 几种常见的凹角微结构如图 3 所示。Fu 等^[64]在不进行表面修饰的前提下, 采用直接激光干涉打印 (Direct laser interference printing) 的方法, 分别在聚对酞酸乙相二酯 (PE) 和聚甲基丙烯酸甲酯 (PMMA) 衬

底上制造了周期性的微柱阵列结构。在不改变表面化学性质前提下, 仅在微观结构的作用下就改变了表面润湿性。此外, Kang 等^[65]制备了一种具有蘑菇状微柱阵列的超双疏表面, 对水和矿物油均表现出了易滑动的特性, 水滴在其表面的 CA 和 SA 分别可以保持在 160° 以上和 20° 以内。相比于单一的圆柱形阵列 (图 4(a)), 蘑菇状阵列表面 (图 4(b) 和图 4(c)) 对液滴表现出了更加优异的抗渗透能力^[66-68]。具有凹角结构的表面经过表面化学改性后具备了超双疏性, 而单一的微柱经过相同处理后却不能实现^[15], 表明了蘑菇头凹角结构在实现超双疏性能方面起着重要作用。此外, 与单层凹角结构相比, 多层凹角结构使其表面的液体难以渗透到内腔中, 不易从 Cassie 态转变到 Wenzel 态, 具备更强的抗黏附性和抗渗透性, 从而更可能实现超双疏性^[69]。也有文献指出, 双凹角^[70-71] (图 4(b)) 和三凹角结构^[72] (图 4(d)) 在稳定气垫和增加涂层耐久性方面发挥重要作用。在凹角结构的设计过程中, 可以通过调整结构参数, 使表面保持更稳定的 Cassie 状态。例如, 通过改变悬垂角来提高表面的抗渗透能力, 从而影响其疏液性能^[70, 73]。Liu 等^[74]利用激光和电化学结合的方法, 在金属基体表面制备了微纳复合的凹角结构, 经化学改性后实现了表面的超双疏。与无规则的粗糙多孔结构相比, 规则微结构的表面通常具有更优异的疏液性, 但制备该结构需要精密的加工设备和精细繁琐的制备工艺。此外, 为了提高表面疏液性, 需要尽可能降低液-固接触面积分

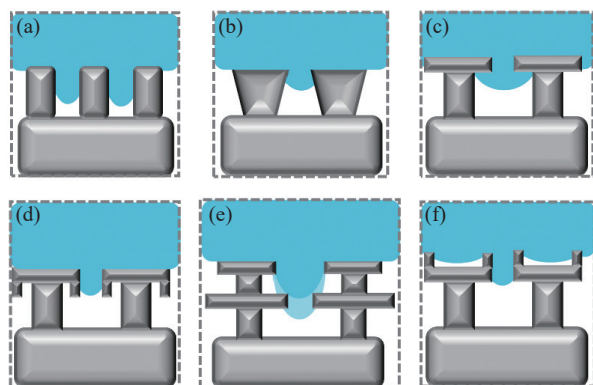
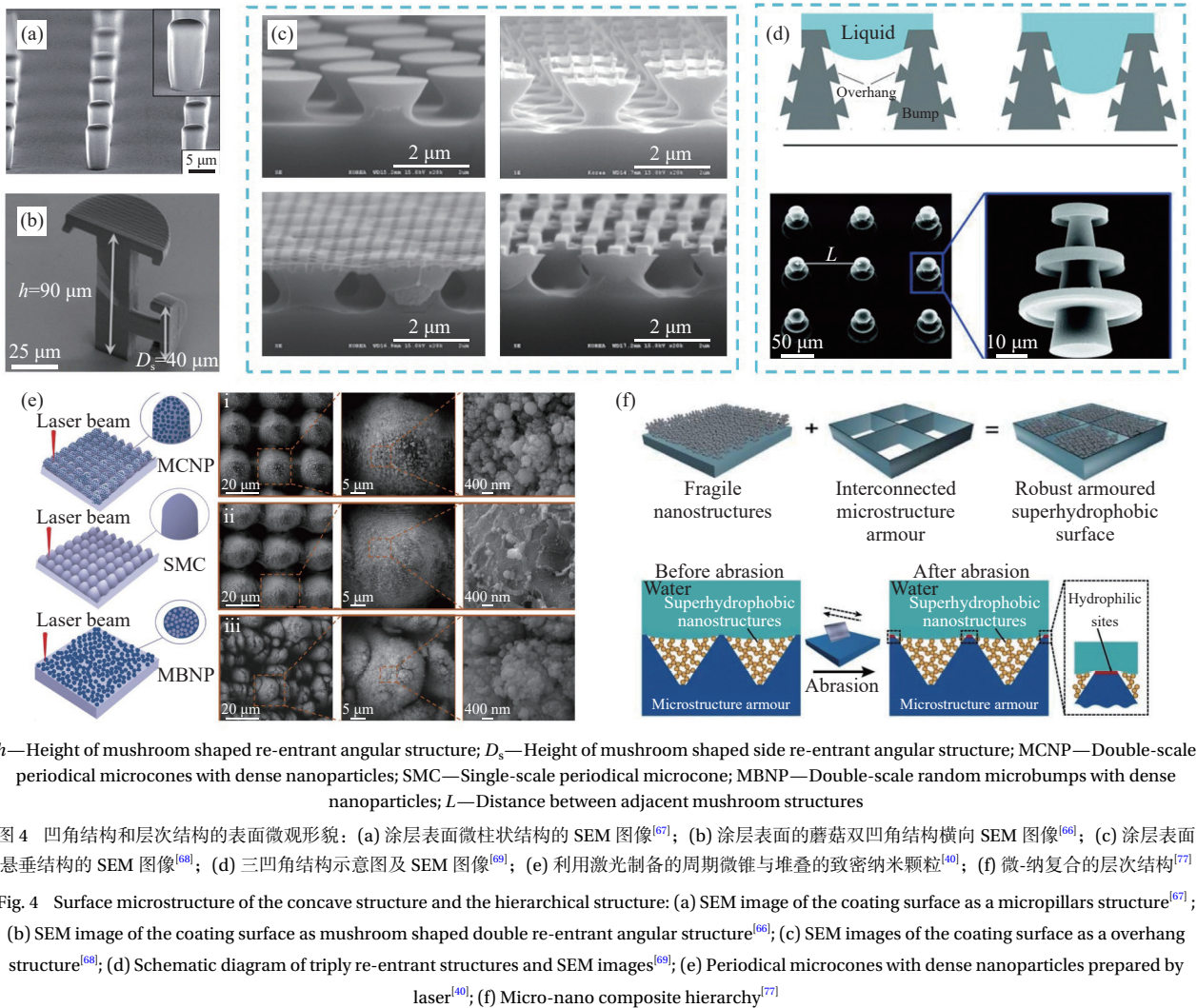


图 3 6 种类型的凹角结构示意图: (a) 微柱; (b) 倒梯形; (c) T 形凹角; (d) T-型折边凹角; (e) T-型双层凹角结构; (f) 带凸角的蘑菇状结构

Fig. 3 Six types of re-entrant structure diagram: (a) Micro-pillar structure; (b) Inverse-trapezoidal structure; (c) T-shape re-entrant structure; (d) T-shape with folding edge re-entrant structure; (e) T-shape double re-entrant structure; (f) Mushroom shaped re-entrant structure with convex edge



h —Height of mushroom shaped re-entrant angular structure; D_s —Height of mushroom shaped side re-entrant angular structure; MCNP—Double-scale periodical microcones with dense nanoparticles; SMC—Single-scale periodical microcone; MBNP—Double-scale random microbumps with dense nanoparticles; L —Distance between adjacent mushroom structures

图4 凹角结构和层次结构的表面微观形貌: (a) 涂层表面微柱状结构的 SEM 图像^[67]; (b) 涂层表面的蘑菇双凹角结构横向 SEM 图像^[66]; (c) 涂层表面悬垂结构的 SEM 图像^[68]; (d) 三角凹角结构示意图及 SEM 图像^[69]; (e) 利用激光制备的周期微锥与堆叠的致密纳米颗粒^[40]; (f) 微-纳复合的层次结构^[77]

Fig. 4 Surface microstructure of the concave structure and the hierarchical structure: (a) SEM image of the coating surface as a micropillars structure^[67]; (b) SEM image of the coating surface as mushroom shaped double re-entrant angular structure^[66]; (c) SEM images of the coating surface as an overhang structure^[68]; (d) Schematic diagram of triply re-entrant structures and SEM images^[69]; (e) Periodical microcones with dense nanoparticles prepared by laser^[40]; (f) Micro-nano composite hierarchy^[77]

数。然而，减少固体区域可能导致微观结构力学性能减弱，难以抵御外部干扰并维持稳定的界面物理特性。因此，在设计超双疏表面的微观结构时，必须同时考虑其耐久性和疏液性，以确保其在实际应用中的稳定性和可靠性。

2.3 层次结构

微-纳米层次结构 (Hierarchical structure) 又称为双尺度微-纳层次结构，可促进表面保持稳定的 Cassie 状态。Nepal 等^[75]的研究表明：层次结构在促进复合材料的耐久性和鲁棒性方面起着至关重要的作用，具有抵抗变形、提高塑性和增强韧性的能力。此外，层次结构也是构建超双疏表面的常见类型。以 Chen 等^[76]的研究成果为例，他们通过运用化学蚀刻技术来生成微米级结构，并借助阳极氧化技术，在微米级结构上进一步构建纳米粗糙结构，从而构造了稳定耐久的微-纳结构。图 4(e) 所示的层次结构是通过慢速激光扫描

与快速激光扫描方式相结合，在表面刻蚀出周期性的微锥结构和纳米级粗糙结构，形成微-纳层次结构^[40]。在缺乏有效保护和修复措施时，纳米粗糙结构极易受到外界物理刮擦和化学腐蚀的破坏，进而对其表面疏液性产生不利影响。而层次结构中较小尺度的结构具有优异的液体拮抗功能，较大尺度的结构则具备保护功能，使表面更加坚固耐用。Wang 等^[77]采用刻印的方式，在金属、玻璃、陶瓷等表面刻印出规则的倒金字塔空腔，然后加入表面能较低的纳米颗粒以形成复合层次结构，如图 4(f) 所示。在机械力的作用下，微米级的倒金字塔空腔结构优先被破坏，从而保护了内部空腔中的纳米颗粒，使表面在保持超疏水性的同时，具备良好的力学稳定性。Zhao 等^[78]利用阳离子氟碳表面活性剂 (Zonyl 321) 与带负电的乳胶颗粒形成复合的粗糙结构，其正负离子结合产生的壳核结构与乳胶颗粒的粗糙结构对超双疏表面

的制备起到了至关重要的作用。因此在涂层表面微结构的实际设计中,可以在涂层表面上集成两种尺度的微观结构,以提高表面的疏液性。例如,经过激光烧蚀加工规则微米大小的凹槽后,采用两步电沉积的方式,在微米级锥体结构的基础上构建了亚微米和纳米锥体结构,形成了微-纳层次结构。这种有序微结构与随机纳米结构相结合,为超双疏表面的制备创造了微结构条件^[74]。

3 化学改性

众所周知,在疏水性表面增加其粗糙度,有利于提高表面疏水性。因此可通过在涂层中加入纳米二氧化硅等颗粒在表面构筑粗糙结构,进而降低涂层表面能,增强其疏液性^[79]。此外,通过化学改性增强表面疏液性能也至关重要。例如氟硅烷、氟基烷烃化合物等常常是用于降低涂层表面能的首选材料。其氟基团的C—F键强度高、临界表面张力低,并且具有良好的化学和生物惰性,可有效降低表面能^[80]。这主要是由于氟原子的电负性较大、原子半径较小,氟碳原子的共用电子对大大偏向氟原子,而且主链中氟原子沿碳链作螺旋分布,形成了一层紧密的负电荷层,使其他原子很难嵌入。如采用全氟烷烃这类氟基团较多的氟化物修饰后的表面,不仅能够疏水,而且对油性物质也具有较好的排斥性^[81]。相比其他处理方法,氟基化合物处理后的涂层表面具有更加优异的疏液性^[8]。因此,通常将一端带有官能团的全氟烷烃分子沉积到涂层表面来进行化学改性^[56]。例如,1H,1H,2H,2H-全氟辛基三氯硅烷(PFOTS)、1H,1H,2H,2H-全氟十二烷硫醇(PFDSH)、1H,1H,2H,2H-全氟辛基三甲氧基硅烷、1H,1H,2H,2H-全氟辛酸(PFOA)和1H,1H,2H,2H-全氟癸基三氯硅烷(PFDTES)等全氟烷烃及其衍生物被用于涂层表面能的降低^[26]。表面能非常低的氟化合物可以最大限度减少固体与表面有机液体的接触,从而满足超双疏表面的制备要求。例如,Bao等^[82]将超疏水的Cu涂层浸入含有1H,1H,2H,2H-全氟癸硫醇和11-巯基十一烷酸(HS(CH₂)₁₀COOH)的硫醇乙醇溶液中,在超疏水涂层上接枝全氟烷基链和末端羧基,成功制备了具有优异超双疏特性的功能涂层。由此可见,通过结合化学改性和提高表面粗糙度的两种方式,可以有效降低材料表面能并增强表面疏液性,从而实现表面的超双疏。

4 制备方法

关于超双疏表面的构建,一方面是表面微结构的制备,另一方面是化学基团和纳米颗粒的添加。微结构的构筑主要是通过两种途径,一类是在基体表面增加材料的方式构建微结构,另一类是在基体表面“雕刻”,通过去除材料形成凹槽结构。比如激光法、模板法主要是用于构建微观结构,而喷涂法、浸涂法、电沉积法既用于微纳结构的构建,也用于低表面能物质的添加。构建的微米级或纳米级的表面结构,可以促进空气在微孔结构中的滞留,形成气垫结构,使涂层表面保持Cassie态,而低表面能物质对基体表面进行化学改性,降低基体的表面能。在微结构和化学成分的共同作用下,最终实现表面的超双疏^[83]。

4.1 激光法

激光法是一种“自上而下”的加工方法。激光可以在多种材料的表面上烧蚀出微米级或纳米级尺度的结构,如工程塑料^[84]、木材^[85]、纸张^[86]、软木^[87]、玻璃^[88]、金属^[89]的表面。通过控制激光束对材料表面局部集中加热,使材料表面蒸发熔化,达到去除材料的目的。可在材料表面加工出微米级沟壑^[90]、沟槽^[91]、蘑菇阵列^[92]等微观结构,使材料表面具有一定的疏水性或亲水性。此外,激光法还可以与其他微结构制备方法相结合。具体来说,我们可通过激光束在材料表面构建微米级的结构,随后采用化学蚀刻、化学沉积或喷涂等手段,将这些纳米颗粒构建到微米结构上,从而赋予材料表面优异的疏液性^[93]。例如,Meena等^[8]利用红外纳秒光纤激光在铝合金6013表面构筑微纳层次结构,并通过氟基硅烷溶液浸涂,制备出了性能优异超双疏表面。激光加工方法具有时间短、成本低、效率高等特点。但激光束在加工过程中会产生大量的热量,不适用于加工小间距的表面和易燃棉织物、橡胶等材料的表面。

4.2 模板法

模板法主要分为两类,一类是以聚四氟乙烯(PTFE)、液体硅橡胶(Liquid silicone rubber)、聚二甲基硅氧烷(PDMS)等液态聚合物为成型材料,浇注于具有微纳结构的表面,经过固化后与基底进行分离,最终形成具有规则微纳结构的“软表面”^[94]。另一类则是通过热压花的方法,通过控制模具的形状,在基体表面压印出所需的阵列结构,可实现低成本、高分辨率和高通量的结构复制^[95]。该

方法可以在硬质材料的表面上制备出如微柱、凹角等周期性的微纳结构,可以满足超双疏涂层对微纳结构的特殊要求。但模具的制备过程相对复杂、精度要求较高、耗时较长、灵活性较差^[64,95-96]。另外,利用特殊掩模部分地遮挡光束,再利用连续的高能电子束、X射线和紫外光去除表面特定部位的物质,从而精确控制表面的微观形貌。但该过程耗时较长,且需要使用精密的光刻设备,成本极高,对加工的材料也有所限制^[97]。

4.3 喷涂法

喷涂法是一种在基材上喷涂功能化颗粒(金属纳米颗粒、金属氧化物纳米颗粒、二氧化硅纳米颗粒等)和聚合物来制备超疏水/超双疏涂层的方法^[98]。如图5(a)所示,通过喷枪将硅树脂溶液、氟化微粒悬浮液和氟化纳米颗粒悬浮液喷涂到基材表面,表面的颗粒经堆叠后形成微粗糙结构,从而形成稳定的 Cassie 态并表现出疏水性^[60]。Peng 等^[99]通过喷涂开发了一种超双疏涂层,其中环氧树脂用作粘合剂,通过将含氟聚合物与纳米颗粒、共溶剂等混合形成共混物,经雾化后喷涂到基材表面,即可在表面形成超双疏涂层。喷涂法构筑的表面微观结构多为粗糙多孔结构,结构特征并不明显,难以满足超双疏表面对微纳结构的苛刻要求,而且微小的液滴容易渗入,无法保持稳定的抗渗透能力^[100-101]。若要实现表面的超双疏特性,则需要使用更复杂的喷涂工艺。例如,通过“Layer-by-Layer”(图5(b))的方法喷涂树脂层、氟化微粒层和氟化纳米粒子层,在构造复杂

的微-纳层次结构同时,尽可能地降低了基体表面能,从而实现了表面的超双疏。Li 等^[102]基于十七氟癸基三乙氧基硅烷(FAS)改性的二氧化硅气凝胶颗粒(F-SiO₂)及氟基化合物聚偏二氟乙烯-共六氟丙烯(Polyvinylidene fluoride-co-hexafluoropropylene, PVDF-HFP)和 FAS 的悬浮液,通过多次喷涂的方式先后将三者组合在棉织物表面,成功制备了 WCA 大于 170°、OCA 约 158°的超双疏表面。喷涂法具有操作简便、便于规模化和工业化生产的特点,是最常用的一种超双疏表面的制备方法^[103-106]。但该方法需要严格控制喷涂距离、喷涂时间、粒子浓度及粒子大小,才能获得理想的超双疏涂层^[98]。而且喷涂在表面的纳米颗粒附着力差,容易在物理刮擦的过程中从基材表面脱落,丧失其超双疏特性。通常需要在涂层材料中加入一定比例的粘合剂(例如环氧树脂和丙烯酸聚氨酯),以增强纳米颗粒与基体表面的附着力,提高耐久性和坚固性^[107-108]。Wei 等^[109]提出了将胶粘剂进行相分离的方法,在避免纳米颗粒嵌入胶粘剂中的同时,也产生了3层的微-纳复合层次结构,有利于通过在涂层和液体的界面处捕获稳定的空气层来增强超双疏性。除此之外,也可以利用液体火焰喷涂(Liquid fire spray)技术制备坚固耐久的超双疏表面^[58,83]。该技术利用液体火焰的高温产生热气溶胶,然后将纳米金属和金属氧化物颗粒固结在金属、陶瓷和其他基底的表面上。沉积纳米颗粒与基体的结合力更强,抵抗机械损伤的能力也更强。



PFOTES—1H, 1H, 2H, 2H-perfluorooctyltriethoxysilane; RP2—Superamphiphobic coating; R1—First spraying coating; RP1—First two spraying coating; PDMS—Poly(dimethylsiloxane); NF—Nanofilament

图5 喷涂法制备的超双疏涂层: (a) 可拉伸超双疏表面上纳米丝结构和分层微/纳米结构的制造工艺示意图^[60]; (b) 通过喷涂技术制备涂层的示意图^[101]

Fig. 5 Superamphiphobic coating prepared by spraying method: (a) Schematic of the fabrication process of the nanofilament-structured and hierarchical micro/nanostructure on stretchable superamphiphobic surface^[60]; (b) Schematic illustration for the preparation of the coatings by the spraying technique^[101]

4.4 浸涂法

浸涂法的基本原理是将基材浸泡在特殊载体配制的溶液中,以液相为介质,在液体表面张力作用下将纳米颗粒转移到基材表面,经干燥固化后,在基材表面形成一层纳米颗粒的涂层。例如,Zhou等^[110]在碱性条件下将正硅酸四乙酯共水解共缩聚制备疏水SiO₂颗粒,分散到含有FAS的聚二甲基硅氧烷(PDMS)/四氢呋喃(THF)溶液中,形成涂层溶液。然后将聚酯织物浸入溶液中浸渍涂层,最后经过高温固化,可在织物表面形成超疏水涂层。该涂层具有优异的疏水性,涂层表面的WCA为171°,滑动角为2°。另外,溶液类型、拉拔速度、浸泡时间和改性添加剂等因素均会影响涂层的疏水性、黏附性、热稳定性和化学稳定性^[111]。例如改变溶液中化合物的配比,将改变涂层表面疏水性和疏油性。Liao等^[112]借鉴水转移打印(Water transfer printing)技术,将疏水亲油的聚丙烯(PP)和疏水疏油的聚四氟乙烯(PTEF)形成混合溶液,利用浸涂法在铜片表面制备超双疏涂层。当PP和PTFE的混合比例控制在1:9和1:10时,涂层表现了超双疏性。Zhao等^[78]将带正电荷氟碳表面活性剂(Zonyl 321)与带负电荷的氟基硅烷改性的聚偏二氯乙烯乳胶颗粒进行自组装,两者通过离子相互作用形成壳核结构,并分散在水中。然后,将壳核结构通过浸涂的方式移植到基材表面,形成超双疏表面涂层。相比于单一的疏水涂层,超双疏涂层需要混合两种或两种以上的聚合物形成复合体系^[13],再移植到基体表面形成超双疏涂层。浸涂法具有成本低、易于实现的优点,但涂层厚度受溶液中离子浓度的影响,可控性较差。

4.5 电沉积法

电沉积是指简单金属离子或复合金属离子通过电化学过程在基材表面形成镀层的过程。阳极和阴极浸泡在含有金属离子的电解液中,阳极氧化,待涂覆的基材往往被还原为阴极,使金属离子沉积在其表面形成涂层^[60]。电沉积技术通过导电基板上吸附带电颗粒实现多尺度结构的构建及表面的化学改性,从而构建超双疏涂层。Li等^[113]分别将铜板和钢试样作为阳极和阴极,利用电沉积的方法在管道钢基体上制备了CuO薄膜。该薄膜表面由纳米片构成,呈现微花状的分层结构,经全氟辛酸(PFOA)低表面能材料改性后,形成了具有自清洁性和耐腐蚀性的超双疏性涂层。He

等^[114]将表面镀有Ag薄膜的聚酰亚胺(PI)作为阴极,分别放入Ce、Mg和Cu基化合物的溶液中进行电沉积,在阴极表面形成了不同种类的微纳米复合的粗糙结构。3种不同涂层的表面均表现出了超疏水性(Ce、Mg和Cu的WCA分别为159.7°、157.0°和153.8°)。Liu等^[74]采用电沉积工艺,在激光制备的微米级锥体结构上制备了亚微米级和纳米级锥体结构,纳米锥结构在微米锥结构的顶部和侧面交替生长,最终形成超双疏表面所需微纳结构。电沉积技术在基体表面形成超双疏涂层是一种简单有效的方法,但电沉积过程中需要消耗大量的电能,并不环保,而且电沉积涂层的性能与沉积金属的性质、电解液的组成、反应温度、电流密度等因素有关,需要专门的设备和技术支持才能保证其可控性^[115-116]。

4.6 刻蚀法

刻蚀法的两种常用方法包括化学试剂刻蚀和离子刻蚀。这两种方法都会与被蚀刻物表面发生化学反应,形成新的化学键和产物,并在扩散作用下,进入表面的溶液或气体中,从而去除表面物质并形成粗糙结构。两者的不同之处在于,化学试剂刻蚀通常使用酸性化学试剂来刻蚀金属等表面,而离子蚀刻则是通过活性粒子轰击并蚀刻表面。Zhao等^[117]将Al片置于CuCl₂水溶液中,在Al表面刻蚀出微米级的结构,然后通过热水浴处理生长出了纳米级纤毛,形成了多层次的微-纳复合结构,再经过氟化烷基磷酸改性处理后,最终获得了具有超双疏性的铝表面。与化学刻蚀相比,等离子体刻蚀可以改善薄膜的润湿性和黏附性能。通过等离子体修饰,涂层或基体表面被烧蚀,产生凹坑和凸峰,其形态受离子浓度、离子能量等因素影响^[118]。等离子体处理在纺织纤维上引入了足够的自由基和官能团,从而单独促进氧化聚合,聚合物与等离子体处理过的纤维发生化学结合,并以黏附沉积的方式在表面形成涂层。Zhang等^[119]采用了一种具有高效益和灵活性的方法,将深度反应离子蚀刻(Deep reactive ion etch)方法与掠角沉积(Glancing angle deposition)工艺相结合,在微米级结构之上构建了纳米级结构,以实现超双疏表面微纳米复合结构的构建。此外,等离子体蚀刻在对基材表面进行化学改性的同时,具有一定的物理效应,可以提高涂层表面的热稳定性和机械稳定性^[120-122]。

4.7 溶胶-凝胶法

溶胶-凝胶法一般通过预先制备的前驱体在液相中进行混合,水解缩聚后形成溶胶体系。此后,溶胶经过聚合、干燥和固化,即可在表面形成具有微纳结构的涂层。利用 SiO₂ 纳米颗粒溶胶-凝胶合成反应技术相对成熟,可以制备出性能优异、功能丰富的超涂层^[123-124]。Lin 等^[125]利用溶胶-凝胶化学方法,将 PDMS-SiO₂ 和聚磷酸铵 (APP) 结合在一起,在织物表面制备了一种耐热的超疏水涂层。Aslan 等^[126]利用溶胶技术在钛金属表面浸涂氧化钛的溶胶,经热处理后形成多孔粗糙的 TiO₂ 薄膜,并以此来构建超双疏表面。溶胶-凝胶法可以实现不同的化学反应,并且具备生产各种纳米/微观结构的能力,这些结构可以在不同形态的微纳米尺度上实现,且方法相对简单,成本也较低,适合于大面积和复杂形状的基材。不过溶胶-凝胶法也存在耗时长、制备效率低、力学性能差等缺陷。

5 应用

5.1 防腐蚀

超双疏表面的固体和腐蚀性液体之间存在空气层,可以有效地防止液体接触固体表面和渗透到微纳米结构和底层基材中,因此,气垫的稳定性对决定其抗侵蚀能力起着关键作用^[24]。图 6(a)展示了在浸泡试验和中性盐雾试验中,涂层通过阻断水或气体,减缓氧和氯离子的扩散,阻碍了镁合金表面的阴极氧还原反应,有效保护了镁合金基体^[127]。Liu 等^[128]利用硅酸镁纳米管 (MS-TNs) 对十二烷基三甲氧基硅烷 (DTMS) 进行改性,作为装载 2-巯基苯并咪唑 (2-MBI) 的纳米容器,在 AZ31 B 镁基体上制备保护涂层 (图 6(b))。MS-TNs/DTMS 粉末制备的涂层具有良好的疏水性,可以阻断液体与固体的接触,从而提高金属表面的抗腐蚀能力。对于常见金属碳钢来说,其表面呈现亲水性,被腐蚀性液体润湿后更容易发生腐蚀,而在碳钢表面制备超双疏涂层可以同时保护碳钢免受腐蚀性溶液和有机液体的污染。Zhang 等^[129]通过将改性的 1H, 1H, 2H, 2H-全氟癸基三乙氧基硅烷修饰的氧化铝纳米颗粒 (Al₂O₃@PDFTES NPs) 喷涂到黏性层上,成功在 Q235 碳钢基材上获得了一种具有自清洁、耐腐蚀的超双疏涂层。经过电化学阻抗谱及动电位极化曲线的测试验证,该涂层展现出了对钢基体的有效保护作用。酸、碱

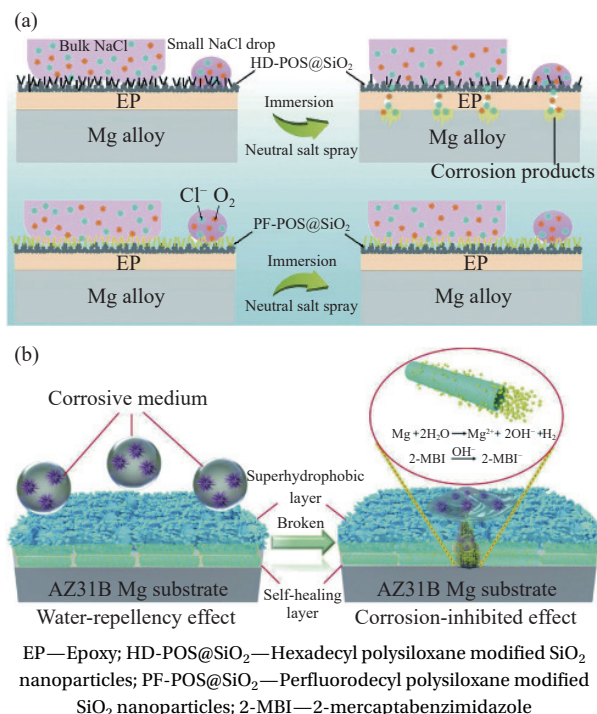


图 6 基于超双疏表面的防腐蚀策略: (a) 表面保护过程示意图^[127]; (b) AZ31B Mg 基双功能涂层的防腐机制^[128]

Fig. 6 Anti-corrosion strategies based on superamphiphobic surfaces: (a) Schematic illustration of the process of surface protection^[127]; (b) Anticorrosion mechanisms of the prepared dual-functional coating for AZ31B Mg substrate^[128]

性液体及卤化物溶液会加速 Al₂O₃ 氧化层及金属基体的腐蚀^[130]。为了缓解腐蚀液体对铝合金的腐蚀, Zhang 等^[6]利用 HCl 刻蚀构建表面微结构,并通过 1H, 1H, 2H, 2H-全氟辛基三乙氧基硅烷对表面进行化学改性,成功制备了 5083 Al 合金超双疏表面。该样品经过 pH 值范围为 1 至 14 的溶液浸泡后,依然能够保持超双疏性 (WCA 均高于 165°, SA 均低于 4°), 表现了良好的抗腐蚀能力。

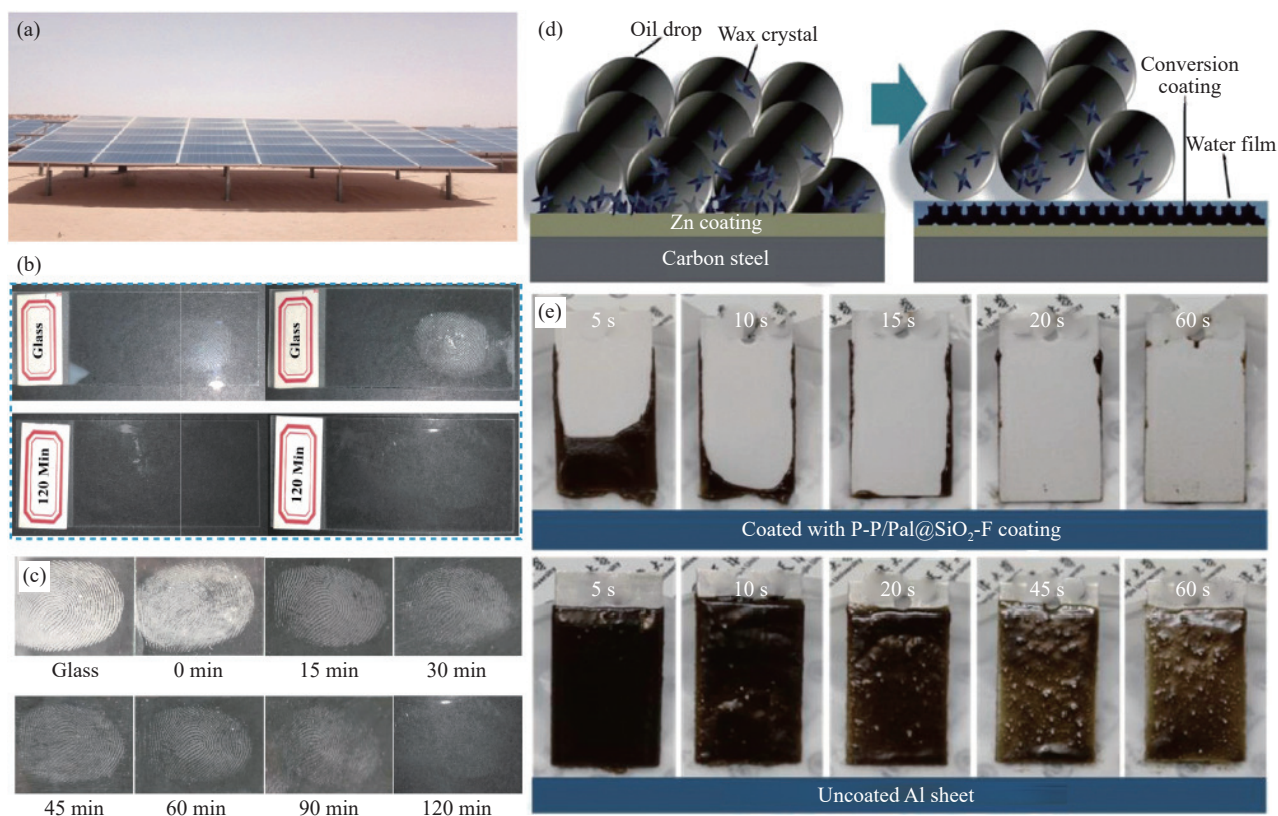
5.2 防污与自清洁

防污与自清洁的应用一直是超双疏涂层研究的热点之一。一方面,超双疏表面对水和油均具有良好的排斥性,不易粘黏液体污物;另一方面,较低的 SA 使液滴更容易在表面滚动,而滚动的液滴可以溶解或携带表面的固体颗粒,实现表面的自清洁。因此,对于油性环境中的电器设备,可利用超双疏涂层实现对无法擦洗部位的自清洁,从而使该部位免受水、油等液体的侵蚀。例如, Liu 等^[131]采用喷涂法在芳纶织物 (AF) 上制备了超双疏表面。涂层中的聚 1H, 1H, 2H, 2H-全氟癸基三氯硅烷 (PFCS) 使超双疏芳纶织物 (SAF) 具有良好的阻燃性和超双疏性 (水为 161°, 油为 155.5°),

可有效防止油类有机物对织物的侵蚀。Jiao 等^[132]通过喷涂树脂底漆,然后将功能化的纳米颗粒浸涂在底漆表面,成功制备了一种抗油液渗透的纳米多孔超双疏涂层。该涂层能够有效抗油液的侵蚀,并且浸泡于 50℃ 的合成油和植物油中 80 d 后,依然能够保持稳定的超双疏性,有望成为隔油池、厨房通风叶轮和厨房排气管上的防污涂料。

透明的自清洁涂层可以应用于建筑物的窗户表面和光学设备屏幕或镜头的防污^[16]。尤其是室外安装的太阳能板表面存在粉尘堆积的问题(图 7(a)),导致透光率呈现明显的下降^[133],人工

清理的成本较高,而具有良好透光性、自清洁性的超两疏涂层的应用可替代人工清理,降低维护成本。另一方面,在光学反射层表面叠加超双疏性,可以使该表面具备良好的防污性的同时保持较高的太阳反射率,减少建筑或玻璃表面对太阳能的吸收,实现被动辐射冷却^[134],降低空调制冷设备的能耗,从而促进节能减排。Liu 等^[135]制备的一种具有辐射冷却功能的超双疏涂层,该涂层对太阳反射率为 98.6%,在保证良好的光学反射性质的同时,还具备了良好的自清洁功能,从而降低灰尘堆积对反射率的影响。



PFDTs—1H, 1H, 2H, 2H-perfluorodecyltrichlorosilane; ChNFs—Chitin nanofibers; Pal@SiO₂-F—Fluorinated palygorskite@SiO₂; PES—Polyethersulfone; PVDF-HFP—Vinylidene fluoride-co-hexafluoropropylene

图 7 自清洁与抗污的应用: (a) 太阳能板上的灰尘堆积现象^[133]; (b) 对比 ZnO 粉末喷涂前(左)后(右)和 PFDTs 改性 ChNFs 涂层在玻璃玻片上指纹的时间变化^[137]; (c) 涂层的指纹图谱时间变化对比^[137]; (d) Zn 涂层的抗粘附过程示意图^[136]; (e) 未涂覆和涂覆 PES-PVDF-HFP/Pal@SiO₂ (P-P/Pal@SiO₂-F) 涂层的 Al 板抗蜡试验照片^[26]

Fig. 7 Self-cleaning and anti-fouling applications: (a) Dust accumulation on solar panel^[133]; (b) Comparison of the fingerprints on glass slide before (left) and after (right) sprinkling ZnO powder and the ChNFs coating modified with PFDTs deposition for time change^[137]; (c) Comparison of time change of coating fingerprint^[137]; (d) Schematic diagram of anti-adhesion process of Zn coating^[136]; (e) Photographs of anti-waxing tests on Al sheet uncoated and coated with PES-PVDF-HFP/Pal@SiO₂ (P-P/Pal@SiO₂-F) coating^[26]

随着指纹识别技术的发展,防指纹触摸屏涂层方面的研究也逐渐引起了学者们的关注。王威等^[136]在手机玻璃表面设计的仿蝉翼超双疏涂层,具有良好的抗指纹特性,能够有效减少手指皮肤

表面的油脂对光学屏幕的污染。Wang 等^[137]首先制备了一种具有亲水性和疏油性的几丁质纳米纤维(ChNFs)超双疏性涂层,保持透明性的同时,还具备了抗指纹特性(图 7(b)和图 7(c))。日常使

用过程中,超双疏涂层在受到刮擦或紫外线照射后表面粗糙结构被破坏,疏液性和透明度会出现下降^[138]。因此,有学者在坚固耐久的透明超双疏涂层的开发方面做出了努力和尝试。Chansomwong等^[139]利用氧等离子体法和正硅酸乙酯 (TEOS) 衍生的 SiO₂ 底漆处理,获得了氟硅烷处理的环氧-硅氧烷杂化透明涂层,经过 5 000 次钢丝绒和 2 000 次橡皮擦磨损试验,该涂层表面仍具有 110°左右的 WCA,展现了良好的耐磨性。

在光学镜片、风挡玻璃和带有亲水材料的玻璃表面,容易附着在表面的雾滴会造成严重的光散射,导致光学镜片透明度下降。例如,医疗领域亲水的内窥镜的镜片容易被人体内的体液、油脂和生物细胞所污染,对诊断过程产生了一定的干扰。超双疏涂层中的纳米颗粒和氟化剂能抑制微生物的生长,而微结构形成的空气垫可以减少生物细胞的黏附面积^[140-141]。Li等^[142]设计了一种具有高透明度、防雾、防血栓特性涂层的镜片。该镜片在血液中反复浸渍 100 次后,仍能保持清洁,且具有优异的抗菌性能,对金黄色葡萄球菌和大肠杆菌的抑菌率分别为 75.7% 和 76.3%。

原油在输送过程中,溶解在热原油中的蜡、胶和沥青等物质会在管道壁上沉淀沉积,并随着管道压力和温度的降低而在管道表面沉淀^[143]。特别是在温度较低的地方,由于管内外温差的存在,管内的蜡沉淀效应更明显^[144-145]。输油管道中蜡质沉积造成的流动堵塞,不仅降低了输油效率,还存在着导致管道断裂和设备损坏的安全隐患^[146-147]。未处理的金属表面原油容易黏附并出现蜡沉淀,而超亲水/水下超疏油涂层的表面可以吸附水膜,在水膜和粗糙结构的协同作用下,有效地阻隔了原油(图 7(d)),削弱原油与管壁的相互作用,减缓蜡质沉积的速率。Wang等^[148]制备的超亲水/水下超疏油涂层,可有效防止蜡的黏附和沉积。但此类表面在水膜被破坏后或混合的水分不足以形成水膜时,抗蜡效果会出现下降^[149]。与超亲水/水下超疏油涂层不同的是,超双疏表面不会因水膜的破坏而对疏液性能造成影响。超双疏表面对水和油性污染物均表现出明显的不润湿性,能够有效减弱原油与管壁的相互作用,起到抗原油黏附、抗蜡沉积和抗腐蚀的效果^[150-151]。Peng等^[26]将坡缕石和 SiO₂ 的复合材料 (Pal@SiO₂-F) 氟化改性后,将其整合到聚醚砜 (PES) 和聚偏氟乙

烯-共六氟丙烯 (PVDF-HFP) 上,构建独特的微/纳米相互交织的分层网络结构,制备了坚固的超双疏涂层。与未涂覆的表面相比,该涂层能够在含水和含油环境中形成稳定的空气层,从而抵抗原油和蜡沉积物的黏附,在浸入原油后仍能保持光滑,如图 7(e) 所示。

5.3 防冰

相关研究表明,在航空、航天、交通等领域,大量的冰层黏附容易对航空航天和交通出行带来不利影响^[152-153]。传统的除冰方法有化学除冰^[154]、加热除冰^[155]、机械除冰^[156]等,但在实际应用中往往达不到预期效果,存在能耗高、效率低的缺点。进一步研究发现^[157],通过超疏水材料可有效提高表面防除冰效果。例如,武壮壮等^[158]利用超快激光加工技术在钛合金表面获得了微米级结构,并复合纳米 SiO₂/氟化聚氨酯涂料,成功制备了 WCA 为 158.9°超疏水表面,显著降低了表面覆冰的黏附力。Wei等^[159]将有机硅改性聚酯 (SPET) 和氟化二氧化硅 (FD-POS@SiO₂) 制备悬浮液,喷涂到铝合金板表面,形成具有众多微球及其微聚集体的超双疏涂层。相比于未处理的铝合金表面,该涂层延迟水的冻结时间(延迟了近 2.4 倍),降低结冰的粘结强度(冰黏附应力减小 70%)。相比于超疏水表面,超双疏具有更优异的疏液性能,防冰性能也更优。除此之外,超双疏表面还可应用于既需要防冰但又存在油污风险的场合。

高效防除冰表面的设计主要从抑制冰核形成、延缓冰霜扩展和降低冰层的黏附性等方面出发,研究超疏水表面与界面自由能、微观几何形貌和表面润湿性与接触传热之间的相互关系,具体可归纳为以下几点^[27,156-157,160-165]:

(1) 空腔结构有利于减小微液滴与固体表面的实际接触面积,降低传热速率,阻止微液滴在表面冷凝成核。当表面粗糙度粒径接近临界晶核尺寸时,冰晶的成核率显著降低。另外,接触面积的减小可以降低冰的黏附力,冰层更易从表面滑落;

(2) 超疏水/超双疏表面的空隙存在大量空气,可以起到较好的隔热作用,降低传热速率的效果,从而延缓冻结过程;

(3) 液滴从水冻结成冰的过程中,需要克服凝结成核的能量势垒做功,而表界面自由能与表面润湿性相关,超疏水/超双疏表面通常存在憎水基团,提高非均相冰成核能垒,抑制微液滴的成核。

低温环境和多次冻-融循环可导致 Cassie-Baxter 态到 Wenzel 态的润湿态转变。因此,保持涂层液-空气界面的稳定性或实现 Wenzel 态到 Cassie-Baxter 态的自发恢复,是防冰涂层能够长期保持超疏水特性和防除冰性能的关键^[40,60]。

6 总结

本文首先对表面润湿理论进行了介绍,分析了超双疏性能的表面微纳结构特点,总结了超双疏表面的制备原理和方法,最后综述了超双疏表面的应用领域。近年来,业内研究者在基本润湿理论及超双疏表面设计原理、制备方法和应用研究等方面取得了多项进展。并且随着科学技术的发展和进步,超双疏表面的制备技术将逐渐趋向低成本、批量化及环保化等方面发展。

(1) 相比于反应离子刻蚀等技术手段,喷涂、浸涂等涂层技术施工更加方便且易于批量化推广应用。但涂层表面耐磨性、力学性能和黏附强度仍有待提升。激光技术和模板法可制备复杂表面微结构,实现超双疏性能,但其设计和制备成本较高,加工尺寸受限。因此,为推进超双疏表面的工业化应用和规模化制备,需综合考虑其经济性、耐久性、工艺性等多方面因素,以实现其综合性能的进一步优化和提升。

(2) 涂层的环保性方面,多数的超双疏涂层需要采用氟基硅烷等低表面能物质进行修饰,对生态环境和人体健康具有一定影响。环保性涂层虽然可以实现表面超疏水,但往往达不到超双疏的效果,不能完全替代含氟超双疏涂层材料。因此,探索和研发经济环保的超双疏表面及其制备技术,也是未来发展的一个重要方向。

(3) 相比于超疏水表面,超双疏表面对微纳粗糙结构的要求相对更高,如需要在表面形成多孔粗糙结构、凹角结构及微纳多级粗糙结构等。目前针对超疏水方面的理论研究相对较多,对超双疏表面的深层机制仍需进一步研究和完善。通过系统理论有效指导超双疏表面制备,有效推进超双疏表面的工业应用和技术推广,是业内研究者的共同追求和愿望。

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