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# 木基柔性电子复合膜的制备及其在传感器中的应用



分享本文

王怡仁<sup>1</sup>, 周彤<sup>1</sup>, 王露臻<sup>1</sup>, 吴启静<sup>1</sup>, 李大纲<sup>1</sup>, 金永灿<sup>2</sup>, 陈楚楚<sup>\*1,2</sup>

(1. 南京林业大学 材料科学与工程学院, 南京 210037; 2. 南京林业大学 轻工与食品学院, 南京 210037)

**摘要:** 为拓展木材多功能化及高值化应用, 以轻木为原料, 通过脱基质工艺去除木材基质, 随后干燥处理获得轻木骨架 (WF), 进一步乙酰化改性后干燥可制得乙酰化轻木骨架 (AWF)。利用浸渍法, 将聚二甲基硅氧烷 (PDMS) 弹性体分别引入 WF 与 AWF 制备木基复合薄膜材料 (PDMS/WF 与 PDMS/AWF)。系统性研究乙酰化改性对复合膜形貌特征、力学性能、化学组分及表面亲水性等的影响。结果表明, 乙酰化处理能够有效促进 PDMS 分布于轻木骨架的孔隙结构中, 二者结合紧密, 界面结合性提高。同时, 制得的 PDMS/AWF 木基复合膜具备较好的柔韧性, 沿纤维生长方向断裂拉伸强度达 176 MPa, 韧性约 6.58 MJ/m<sup>3</sup>, 几乎是 PDMS/WF 复合膜的两倍。进一步将该 PDMS/AWF 木基复合膜作为柔性基材, 组装柔性传感器件, 在多种形变下表现出稳定及可重复的相对电阻值变化。预期在智能家居、软体机器人及柔性可穿戴电子等智能响应器件研究领域具有潜在的应用。

**关键词:** 木材; 聚二甲基硅氧烷; 乙酰化; 复合膜; 柔性电子基材; 传感器

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## Preparation of flexible wood-based electronic films and its application for sensors

WANG Yiren<sup>1</sup>, ZHOU Tong<sup>1</sup>, WANG Luzhen<sup>1</sup>, WU Qijing<sup>1</sup>, LI Dagang<sup>1</sup>, JIN Yongcan<sup>2</sup>, CHEN Chuchu<sup>\*1,2</sup>

(1. College of Materials Science and Engineering, Nanjing Forestry University, Nanjing 210037, China; 2. College of Light Industry and Food Engineering, Nanjing Forestry University, Nanjing 210037, China)

**Abstract:** In order to expand multi-function and high-value application of wood, balsa wood was used as raw material. Firstly, they were performed with chemical treatment to remove the matrix including lignin and hemicellulose, followed with drying. The acetylated balsa wood frame (AWF) was prepared by acetylation modification. Afterwards, by vacuum impregnation, polydimethylsiloxane (PDMS) elastomer was introduced into balsa wood frame (WF) and AWF respectively, in order to fabricate composite film materials (PDMS/WF and PDMS/AWF). The effects of acetylation modification on morphology, mechanical properties, chemical composition and surface hydrophilicity of composite films were systematically studied. The results show that after acetylation, the interface between balsa wood frame and PDMS is more compact, and the pores between PDMS and white wood are smaller. At the same time, the tensile strength of PDMS/AWF composite film (along the fiber growth direction, L-direction) is around 176 MPa, and the toughness is about 6.58 MJ/m<sup>3</sup>, which is nearly twice as high as that of PDMS/WF composite film. Furthermore, the prepared PDMS/AWF wood-based composite film was used as a flexible substrate to assemble a flexible sensor. As a result, it shows stable and repeatable changes for relative resistance values under various deformations. Altogether, it has great potential to be applied in the research fields of smart furniture, elastic substrates of smart response devices, flexible electronic components and wearable devices.

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通信作者: 陈楚楚, 博士, 副教授, 硕士生导师, 研究方向为纤维素、甲壳素、复合材料 E-mail: [chuchu\\_chen@njfu.edu.cn](mailto:chuchu_chen@njfu.edu.cn)

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**Keywords:** wood; polydimethylsiloxane; acetylation; composite film; flexible electronic substrate; sensor

木材是一种天然可再生资源,具有结构层次分明、构造复杂有序及多孔结构精细等结构特性,同时具备低密度、高比模量及高比强度等良好的材料性能<sup>[1-3]</sup>。木材细胞壁主要由纤维素、半纤维素及木质素组成,其中纤维素为骨架物质,木质素及半纤维素分别起“固化剂”及“黏结剂”作用,共同形成木材独特的复合结构<sup>[4]</sup>。但由于木材自身缺陷,如尺寸稳定性、热稳定性及耐水性差等问题,使用过程中需对其进行加工改性<sup>[5]</sup>,而其天然的各向异性纤维骨架结构也为木材多功能化应用提供了基础<sup>[6-9]</sup>。

近年来,研究人员分别采用“自下而上”及“自上而下”的方式对木材及其衍生物进行改性及多功能化应用<sup>[6]</sup>。其中,对木材进行纳米化处理<sup>[10]</sup>,通过自下而上的手段可制备获得如木质纳米纤维素丝<sup>[11-13]</sup>、薄膜<sup>[14-17]</sup>及凝胶<sup>[18-20]</sup>等。但纯化纳米纤维素制备过程复杂、成本高,且涉及大量的能源损耗及化学试剂,不利于其进一步规模化应用的发展。自上而下的策略是利用木材的各向异性复合结构,保留木材天然纤维骨架,对木材进行化学处理及功能化改性,可制备获得如木基水凝胶<sup>[21-23]</sup>、木基透明膜<sup>[24-25]</sup>、透明木材<sup>[26-29]</sup>、导电木材<sup>[30-31]</sup>及磁性木材等<sup>[32-34]</sup>。Li等<sup>[26]</sup>对脱基质木材表面进行乙酰化改性处理,从而改善了疏水性聚甲基丙烯酸甲酯(PMMA)与亲水性木材纤维素间的界面结合性,制备获得了透光率近90%的乙酰化透明木材。Foster等<sup>[35]</sup>采用亚氯酸钠与醋酸盐溶液对木材进行脱木质素处理,并进一步实施乙酰化改性后与聚甲基丙烯酸甲酯复合,制得的透明木质复合材料与未经乙酰化处理的样品相比,透光率及雾度均有所改善。以上研究表明,木材纤维骨架与功能性粒子间的界面结合性是影响其复合材料性能的关键因素之一。因此,如何提高二者之间的界面相容性,从而进一步拓展其功能化应用逐渐成为目前研究者亟待解决的关键问题。

本文以轻木为原料,通过脱基质处理制备获得轻木骨架,并通过乙酰化改性降低其纤维素表面亲水性。以上述乙酰化改性轻木骨架为增强相,利用浸渍法在其多孔结构中引入聚二甲基硅氧烷,制备获得木基柔性复合薄膜,并对其微观形貌、化学组分、亲水性及力学性能等进行表征分析。

随后,将该木基复合薄膜样品组装成柔性传感器件,并对其传感性能进行表征。

## 1 实验部分

### 1.1 原材料

轻木(密度:0.16~0.2 g/cm<sup>3</sup>),沿轴向切片制成3 mm×3 mm×1 mm(长×宽×厚)薄片,南京姜华化玻有限公司;184PDMS液体硅橡胶,美国道康宁公司;乙酸、正己烷、高氯酸、甲苯、乙酸酐、乙醇及丙酮等试剂均为分析纯,南京姜华化玻有限公司;亚氯酸钠(80wt%)及NaOH(98wt%),南京姜华化玻有限公司;去离子水为实验室自制。

### 1.2 轻木骨架及其膜材料的制备

配制2wt%的亚氯酸钠溶液,调节pH至4~5。将轻木片(轻木与亚氯酸钠质量比 $m_{\text{轻木}}:m_{\text{亚氯酸钠}}=1:2$ )置于上述酸性亚氯酸钠溶液中,100℃加热2 h后,取出轻木片用去离子水冲洗至中性。配制15wt%的NaOH溶液,将上述酸性亚氯酸钠处理后的轻木片放入其中,40℃浸泡处理2 h,制得轻木骨架(WF),取出后用去离子水冲洗至中性,保存备用。将部分WF置于两片玻璃板间,烘箱干燥,制得WF膜。

### 1.3 乙酰化轻木骨架及其膜材料的制备

取40 mL乙酸、50 mL甲苯、0.2 mL(60wt%)高氯酸溶液混合搅拌均匀,并加入5 mL乙酸酐,混合均匀,配制乙酰化溶液。将上述WF用乙醇、丙酮逐级置换水分后置于乙酰化溶液中,常温条件下浸泡4 h后,随后用去离子水冲洗至中性,制得乙酰化轻木骨架(AWF)。将AWF置于两片玻璃板间,使用长尾夹固定,置于烘箱干燥,制得AWF膜。

### 1.4 聚二甲基硅氧烷(PDMS)溶液的制备

将PDMS与固化剂按照质量比 $m_{\text{PDMS}}:m_{\text{固化剂}}=10:1$ 混合溶解于正己烷中,配制30wt%的PDMS溶液。

### 1.5 木基复合膜的制备

将WF膜与AWF膜分别浸泡至PDMS溶液中,随后置于真空瓶内进行“抽气-放气”循环3次,每次20 s。浸渍完成后取出复合膜,在60℃条件下加热固化2 h,分别制得聚二甲基硅氧烷/轻木骨架(PDMS/WF)复合膜及聚二甲基硅氧烷/乙酰化轻木骨架(PDMS/AWF)复合膜,图1为其制备流程。

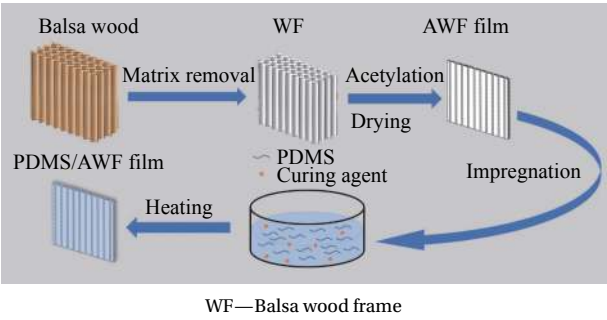


图1 聚二甲基硅氧烷/乙酰化轻木骨架 (PDMS/AWF) 复合膜制备流程示意图

Fig.1 Preparation process of polydimethylsiloxane/acetylated balsa wood frame (PDMS/AWF) composite film

1.6 测试方法

1.6.1 微观形貌表征

使用扫描电子显微镜 (SEM, 型号为 Phenom Pro, 上海复纳科学仪器有限公司)对 PDMS/WF 复合膜及 PDMS/AWF 复合膜表面及断面的微观形貌进行表征分析。将样品在 105℃ 下干燥 2 h 后进行喷金处理, 扫描电压为 1.5 kV, 电流为 10 μA。

1.6.2 力学性能测试

将 WF 膜、PDMS/WF 复合膜及 PDMS/AWF 复合膜分别沿木材纤维生长方向 (L-direction) 与垂直纤维生长方向 (T-direction) 裁剪成 25 mm×5 mm 的样条, 使用万能力学试验机 (SANS, 深圳市新三思材料检测有限公司) 对其进行拉伸性能测试, 使用 1 kN 传感器, 拉伸测试速度为 10 mm/min。试样韧性 (U) 根据应力-应变曲线, 由下式计算得到<sup>[36]</sup>:

$$U = \int_0^{\varepsilon_{\max}} \sigma d\varepsilon \tag{1}$$

式中:  $\sigma$  为拉伸应力;  $\varepsilon$  为拉伸应变;  $\varepsilon_{\max}$  为断裂时的应变。所有数据均以至少五个样本测量值的平均值。

1.6.3 傅里叶红外光谱测试

对样品进行干燥处理后, 使用傅里叶红外光谱仪 (型号为 Nicolet I S10, 美国 Thermo Scientific 公司) 单次反射金刚石探头, 在 Smart i TR diamond ATR 模式下对 WF 膜、AWF 膜、PDMS/WF 复合膜及 PDMS/AWF 复合膜的化学组分进行测试。扫描速度为 4 cm/s, 波数扫描范围为 4000~650 cm<sup>-1</sup>。

1.6.4 水接触角测试

使用 OCA40 全自动单一纤维接触角测量仪 (东方德菲仪器有限公司) 分别对 PDMS/WF 复合膜及 PDMS/AWF 复合膜样品进行水接触角测试。

滴加 50 μL 去离子水至样品表面, 使用高分辨率 1/2"CCD 黑白摄像头观察水滴在其表面的状态, 表征其表面亲水性。

1.6.5 木基柔性电子传感器组装与性能测试

以 PDMS/AWF 复合膜作为柔性基材, 在其表面喷涂导电石墨 (南京先丰纳米材料科技有限公司) 进行封装, 连接导线及万用电表 (UT-803, 优利德科技有限公司) 后组装柔性电子传感器。模拟多种人体活动, 对形变过程中传感器的实时相对电阻变化进行检测并记录。

2 测试方法

2.1 木基复合膜的微观形貌

图2为PDMS、轻木、WF膜、AWF膜、PDMS/WF复合膜及PDMS/AWF复合膜的表面微观形貌图像。可以看出, 脱基质处理后, 木材试样表面呈现疏松且高度定向的纤维排列结构 (图 2(c)), 说明化学处理并未破坏轻木 (图 2(b)) 天然的定向纤维孔道结构。乙酰化改性后, 样品表面形貌更粗糙 (图 2(d))。经过浸渍处理后 (图 2(e)), 样品表面较光滑, 这是由于 PDMS (图 2(a)) 填充于复合膜表面的孔隙结构中。进一步乙酰化改性后所得 AWF 复合膜表面更致密、平整, 说明 PDMS 与木骨架间的界面结合性较好, PDMS 均匀包覆于木材骨架

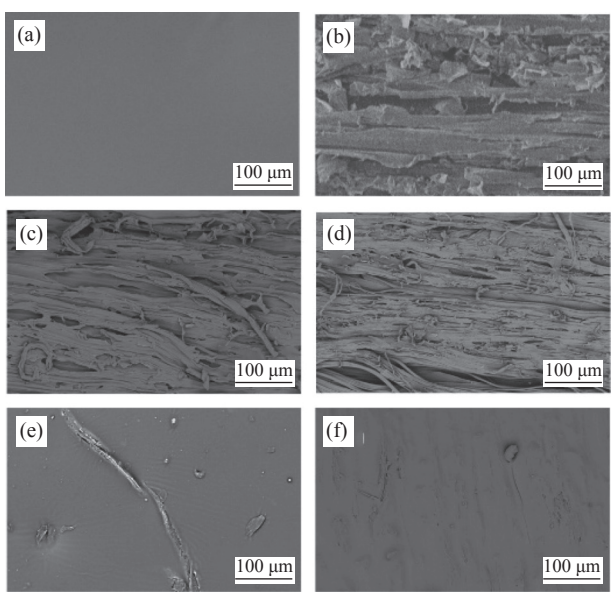


图2 PDMS 及木基复合膜试样表面微观形貌: (a) PDMS; (b) 轻木; (c) WF; (d) AWF; (e) PDMS/WF; (f) PDMS/AWF

Fig. 2 Surface morphologies of PDMS and wood composite film samples: (a) PDMS; (b) Balsa wood; (c) WF; (d) AWF; (e) PDMS/WF; (f) PDMS/AWF



表面，复合膜表面疏水性得到改善。

图3为PDMS/WF复合膜及PDMS/AWF复合膜的断面分别放大2 000倍及5 000倍的SEM图像。WF与PDMS复合后(图3(a)和图3(b))，可观察到复合材料间结构疏松，孔隙较大，这是由于疏水性PDMS与亲水性纤维素间界面结合性较差。而经乙酰化处理后，由于木材纤维素表面亲水性降低，极性减小，使AWF与PDMS复合更加紧密，二者之间孔隙较小(图3(c)和图3(d))。

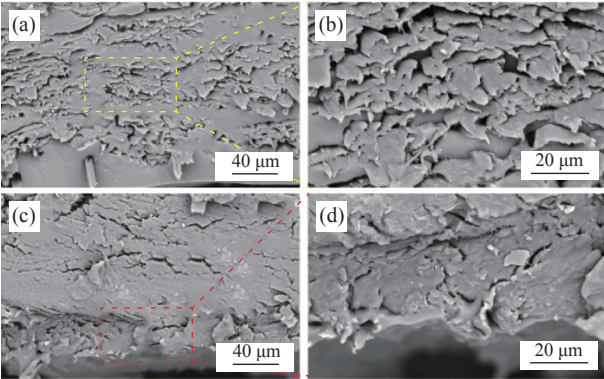


图3 木基复合膜试样断面微观形貌：((a), (b)) PDMS/WF；((c), (d)) PDMS/AWF

Fig. 3 Fracture surface of wood composite film samples: ((a), (b)) PDMS/WF; ((c), (d)) PDMS/AWF

2.2 木基复合膜的力学性能

图4为WF膜、PDMS/WF复合膜及PDMS/AWF复合膜沿纤维生长方向(L-direction)的拉伸应力-应变曲线。与轻木((6.29±0.02) MPa)相比，脱基质处理所得WF膜的断裂拉伸强度((213.26±3.58) MPa)提高了近35倍。这是由于脱基质处理后所得轻木骨架在压缩干燥过程中密实化程度提高。乙酰化处理后所得PDMS/AWF复合膜样品沿纤维生长方向拉伸强度与PDMS/WF复合膜相比，由(164.58±12.65) MPa提高至(176.58±9.89) MPa，断裂伸长率由(3.25±0.35)%提高至(5.71±0.43)%，韧性提高了接近2倍((3.41±0.11) MJ/m<sup>3</sup>提高至(6.58±0.08) MJ/m<sup>3</sup>)，见表1。这是由于AWF表面亲水性降低，作为刚性支撑骨架与PDMS复合，二者之间结合更紧密，复合薄膜的力学性能得到提升。与传统纤维素增

强PDMS柔性复合膜<sup>[37-38]</sup>相比，由于WF的高度定向结构及AWF与PDMS之间较好的界面结合性，使PDMS/AWF复合膜的力学性能有极大的提升。

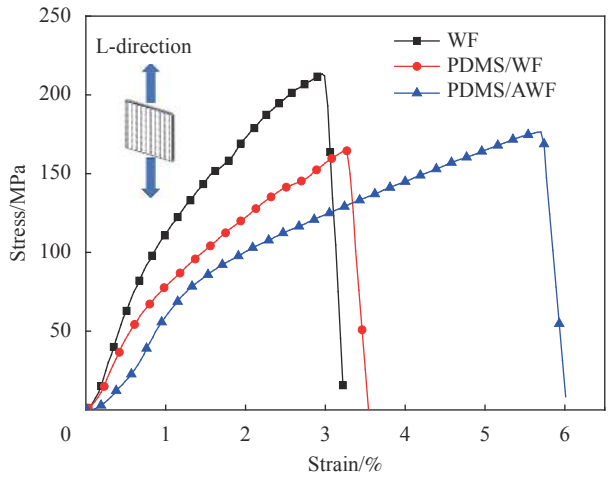


图4 WF、PDMS/WF及PDMS/AWF复合膜沿纤维生长方向(L-direction)拉伸应力-应变曲线

Fig. 4 Tensile stress-strain curves of WF, PDMS/WF and PDMS/AWF composite films along longitudinal direction (L-direction)

图5为PDMS/WF膜及PDMS/AWF膜的垂直纤维方向(T-direction)拉伸应力-应变曲线。可以观察到乙酰化后的PDMS/AWF复合膜与PDMS/WF复合膜相比，T-direction的拉伸强度由(20.68±2.38) MPa提升至(22.59±1.89) MPa。这是由于乙酰化处理后，PDMS与轻木骨架二者之间的界面结合性提高。同时，由于轻木骨架的高度各向异性结构特征，使木材复合薄膜在T方向拉伸强度仅为L方向拉伸强度的10%左右。

2.3 木基复合膜的结构组成

图6为PDMS、WF、AWF及木基复合膜FTIR图谱。与WF膜相比，经乙酰化改性后，AWF膜中位于1 732 cm<sup>-1</sup>处酯类官能团的C=O键振动峰增强及1 239 cm<sup>-1</sup>处酯类官能团C—O—C键振动峰增强<sup>[39-40]</sup>，这是由于表面乙酰化处理后酯类官能团数量增加，木材表面极性降低，亲水性降低。PDMS、PDMS/WF复合膜及PDMS/AWF复合膜曲线中，均在2 962 cm<sup>-1</sup>、1 258 cm<sup>-1</sup>、1 012 cm<sup>-1</sup>与790 cm<sup>-1</sup>处对应出现Si(CH<sub>3</sub>)<sub>2</sub>中C—H的伸缩振动

表1 WF膜、PDMS/WF复合膜及PDMS/AWF复合膜纤维生长方向拉伸应力-应变数值及PDMS在复合膜中质量分数  
Table 1 Tensile stress-strain values of WF, PDMS/WF and PDMS/AWF film along L-direction and the mass fraction of PDMS

| Sample   | PDMS/wt%   | Fracture strength/MPa | Young's modulus/GPa | Fracture strain/% | Toughness/(MJ·m <sup>-3</sup> ) |
|----------|------------|-----------------------|---------------------|-------------------|---------------------------------|
| WF       | 0          | 213.26±3.58           | 12.44±0.05          | 2.93±0.21         | 4.23±0.03                       |
| PDMS/WF  | 53.39±0.65 | 164.58±12.65          | 11.46±0.10          | 3.25±0.35         | 3.41±0.11                       |
| PDMS/AWF | 35.33±2.98 | 176.48±9.89           | 8.99±0.03           | 5.71±0.43         | 6.58±0.08                       |

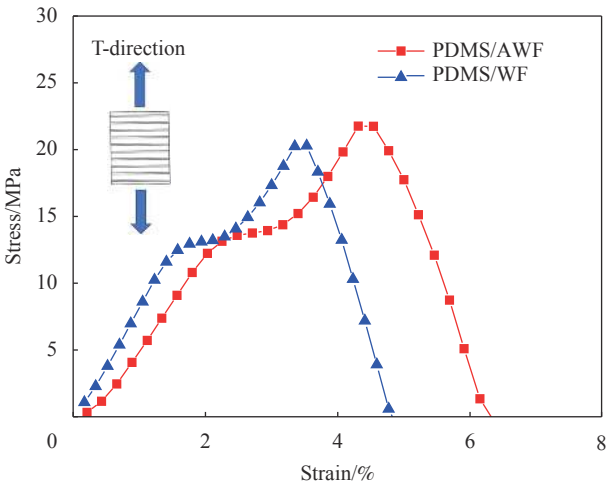


图5 PDMS/WF 及 PDMS/AWF 复合膜垂直于纤维生长方向 (T-direction) 的拉伸应力-应变曲线

Fig. 5 Tensile stress-strain curves of PDMS/WF and PDMS/AWF composite films along perpendicular to the longitudinal direction (T-direction)

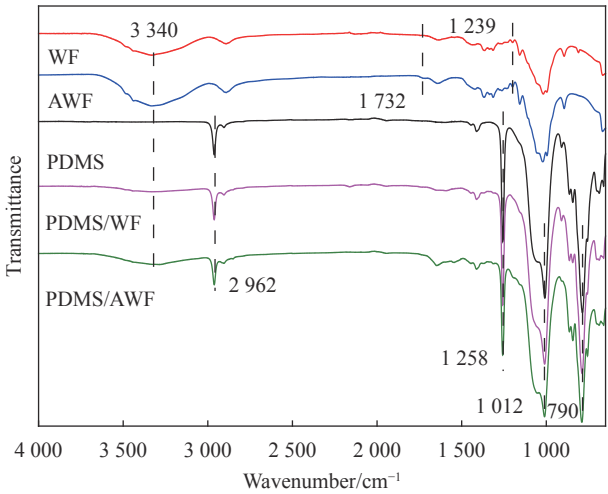


图6 PDMS、WF、AWF、PDMS/WF 及 PDMS/AWF 复合膜的 FTIR 图谱

Fig. 6 FTIR spectra of PDMS, WF, AWF, PDMS/WF and PDMS/AWF composite film

峰、Si—CH<sub>3</sub> 的伸缩振动峰、Si—O—Si 的不对称伸缩振动峰、Si—CH<sub>3</sub> 的弯曲振动峰，均为 PDMS 的特征峰<sup>[41]</sup>。PDMS/WF 复合膜及 PDMS/AWF 复合膜样品的 FTIR 图谱中 3 340 cm<sup>-1</sup> 处表示羟基官能团中 O—H 拉伸振动峰强度降低，是由于复合膜样品表面 PDMS 聚集。

2.4 木基复合膜的表面性能

采用接触角测试仪对乙酰化处理前后所得木基复合膜的表面性能进行表征分析，如图 7 所示。PDMS/WF 复合膜的表面水接触角 (图 7(a)) 随时间

逐渐减小，60 s 后接触角由 82.07° 降低至 63.21°，与未经复合的 WF 水接触角 (<10°) 相比，表面亲水性显著降低。这是由于 WF 与 PDMS 复合后，疏水性的 PDMS 浸入 WF 内部，同时附着于表面，改善了木材表面的强亲水性。但由图 3(a)、图 3(b) 可知，WF 与 PDMS 复合后仍有较多孔隙，导致复合膜表面容易被水润湿。而乙酰化改性处理后，PDMS/AWF 复合膜水接触角 60 s 后，仅由 97.43° 减小至 95.14° (图 7(b))，表面疏水性显著提高。这是由于 AWF 与 PDMS 结合更紧密，复合膜内孔隙较少，水分不易从表面渗透，说明乙酰化处理能够显著改善 WF 与 PDMS 间的界面结合性。

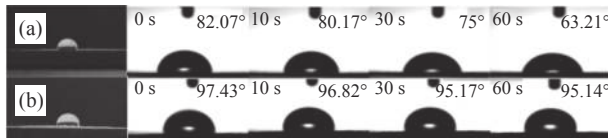


图7 PDMS/WF 复合膜 (a) 及 PDMS/AWF 复合膜 (b) 水接触角测试

Fig. 7 Water contact angle of PDMS/WF (a) and PDMS/AWF (b) film

2.5 木基柔性电子器件应用

图 8 为木基复合膜实物图及组装柔性传感器示意图。可以看出，制备所得 PDMS/AWF 复合膜具有良好的柔韧性，可以弯曲、打结而不发生结构破坏 (图 8(a)、图 8(b))。为了进一步探索制备所得木基复合膜作为基材在柔性电子研究领域的应用，在 PDMS/AWF 复合膜表面喷涂导电石墨 (电阻率为 1.38×10<sup>-5</sup> Ω·m) 制备木基柔性电子复合膜 (20 mm×5 mm×0.099 mm，电阻值为 80 kΩ)，并组装应变传感器 (图 8(c))。

图 9 为监测该木基柔性电子复合膜在发生反复对折弯曲变形 100 次 (图 9(a))、笔尖点击 (图 9(b)) 及笔尖书写 (图 9(c)) 所产生的形变过程中的相对电阻 (ΔR/R<sub>0</sub>) 发生变化，发现应变传感器在循环多次形变下仍能保持稳定的电子信号传输。研究结果表明，制备所得 AWF/PDMS 木基柔性复合膜在柔性可穿戴<sup>[42]</sup>、智能应变传感<sup>[43]</sup>、软

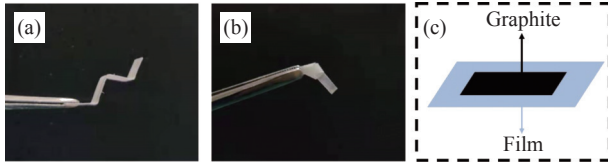


图8 PDMS/AWF 木基复合膜样品折叠 (a)、打结 (b) 和组装柔性传感器 (c)

Fig. 8 PDMS/AWF composite film upon folding (a), knotting (b) and assembling into flexible sensors (c)

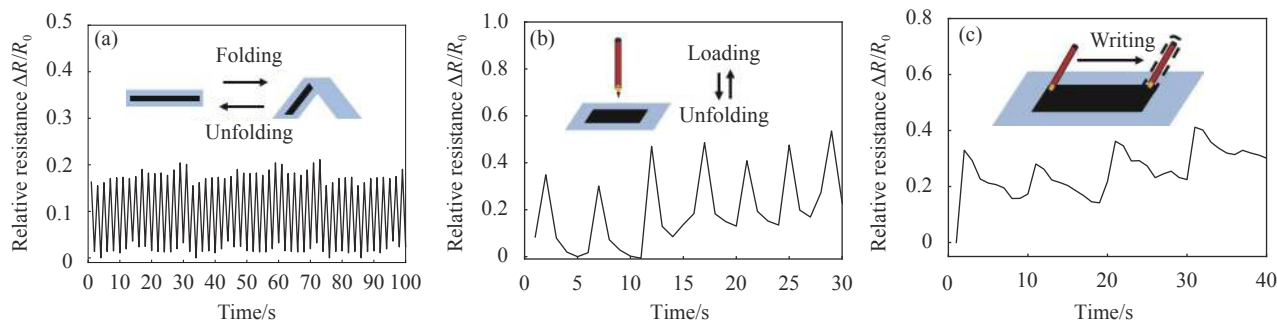


图9 木基柔性传感器弯曲折叠(a)、点击(b)及书写(c)过程中的相对电阻( $\Delta R/R_0$ )变化

Fig. 9 Relative resistance ( $\Delta R/R_0$ ) changes of flexible sensor upon repeated bending (a), clicking (b) and writing (c)

体机器人等智能响应电子器件研究领域具有潜在的应用价值。

### 3 结论

(1) 以轻木为原料, 通过脱基质结合表面乙酰化改性, 将其与聚二甲基硅氧烷 (PDMS) 弹性体复合, 制备获得了一种木基柔性复合膜材料。

(2) 微观形貌分析可知, 乙酰化处理后, PDMS 填充于轻木骨架的孔隙之中, 两者界面结合性显著提高; 水接触角测试表明乙酰化改性提高了复合膜表面的疏水性。

(3) 力学性能测试结果表明, 聚二甲基硅氧烷/乙酰化轻木骨架 (PDMS/AWF) 复合膜的 T 方向断裂拉伸强度可达 176.58 MPa; 与未经乙酰化处理所得聚二甲基硅氧烷/轻木骨架 (PDMS/WF) 复合膜相比, 其韧性提高了 2 倍。

(4) 将上述 PDMS/AWF 复合膜组装柔性电子传感器件, 研究发现其在多种形变下均表现出较稳定的相对电阻值变化。预期可应用于柔性可穿戴、智能传感、软体机器人等柔性智能电子响应器件。

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